

DOWNHILL SKI

The present invention relates to a downhill ski.

As shown schematically in Figure 1, every ski is known to present a camber, i.e. a downwardly concave curved longitudinal profile, so that when it rests in an unstressed state on a surface, it is raised in its central region 1 (between the heel fixing unit T and the front jaw P of the binding), compared with the tail 2 and shovel portion 3, i.e. the section 4 where the tip curvature commences.

This camber ensures stability during straight-line skiing, however when associated with a certain flexural rigidity it can penalize manoeuvrability along curves. In this respect, when the skier travels through curved trajectories, assuming that inclined position to achieve a state of instantaneous dynamic equilibrium induced by centrifugal force, the ski no longer adheres to the ground flatly, but instead along its laminated edges and has to counter-flex to assume an elastic deformation with downward convexity (Figures 2, 3).

The shape of this elastic deformation assumed by most commercially available skis resembles a circular arc (line C of Figure 2). Experimental trials have shown that during initial access to the curve and then during travel along it, the ski obtains a decided advantage in terms of adherence to the ground, lateral holding, stability and slidability by a shape which, along the front portion of the ski, resembles an elliptical arc much more than a circular arc (line E of Figure 2), i.e. the elastic counter-flexural deformation concerns the front portion of the ski much more than the central portion 1, to an extent which increases towards the shovel portion 3.

This theory emerges more rationally on examining the distribution of the ground reaction load on the laminated edge of the ski when in an angled position. This distribution (confronting the gravitational and centrifugal action F of the skier) must adequately involve the entire length of the ski, including its ends, particularly
5 the front end, in a sufficiently regular form and to a significant extent (full line in the example of Figure 4), rather than disproportionately to an insignificant extent (dashed line of Figure 4), as happens in the majority of commercial products (even those intended for sporting and/or competitive use).

There is in fact an increasing tendency to give the ski a considerable
10 softness, with a consequent unfortunate concentration of the reaction load at the centre (dashed line of Figure 4). The ability to load the ends is therefore based on a very wide sidecut configuration at the tail and in particular at the shovel portion, in accordance with known carving skis. However this expedient, combined with the said basic softness, results in a load distribution in no way equitable and
15 progressive, but in fact incongruously disproportionate, i.e. an excessive absolute maximum at the centre, excessive relative end maximums, and intermediate regions of almost zero load (dashed line of Figure 4).

In effect, if only the geometry (sidecut) is varied, a sufficiently effective reaction load distribution can be achieved by giving the ski a considerable rigidity
20 (hence penalizing manoeuvrability, adherence to the ground and slidability). In contrast, in the case of adequately flexible skis, a partial improvement can be achieved by using an interface plate between the ski and boot, to transmit the skier's action to it in a less concentrated manner. As shown schematically in Figure 5, a plate fixed to the ski close to its ends can divide the load F exerted by

the skier into two forces, F' and F'' , so beneficially influencing the reaction load distribution. A substantially similar effect could be achieved by a plate fixed to the ski by supports providing more or less large-area or totally continuous contact. In all cases the benefit can only mainly (or exclusively) concern the central region of the ski, and only marginally involve (or not involve) the shovel portion.

If a more involved design in terms of elasticity is to be attempted, the ski must be made rigid along a considerable length of the central region and of that portion behind the front jaw, to then suddenly become flexible by abruptly tapering its thickness in proximity to the shovel portion.

However this can penalize the equipment in terms of fragility and twistability. Hence a structure must be used which is suitable only for the highest level (exclusively reserved for high-level competition), with excessively sophisticated design and production procedures, in contrast to modern requirements of industrial efficiency and economy.

The object of the invention is to overcome these contradictions by providing a ski having adequate flexibility with good reaction load distribution.

This object is attained according to the invention by a downhill ski as described in claim 1.

A preferred embodiment of the present invention and some variants thereof are described in detail hereinafter by way of non-limiting example with reference to the accompanying drawings, in which:

Figure 1 is a side view of a traditional ski,

Figure 2 shows it while undergoing a curve,

Figure 3 shows a skier while undergoing a curve;

Figure 4 shows the reaction load distribution diagram,

Figure 5 shows a ski provided with a plate in accordance with the known art,

Figure 6 shows a ski according to the invention,

Figure 7 shows the plate in detail, and

5 Figures 8 to 17 show variants of the ski.

As can be seen from Figures 6 and 7, the ski of the invention comprises an elastic compensation superstructure provided with a special front constraint in the form of a more complex innovative plate composed not only of the traditional base member (connected to the centre of the ski) but also of a front prolongation 5
10 which reacts against the (aforedescribed) counter-flexure with a downward thrust F_{spat} on a point 6 situated around the middle of that ski portion between the front jaw P and the section 4 (where the tip curvature commences).

The connection of the ski to the front end of said elongated plate at the point 6 must satisfy precise fundamental connection conditions, allowing freedom
15 of rotation about a transverse-horizontal axis, and freedom of longitudinal sliding, so that no limitation is imposed on the flexibility of the shovel portion itself. This means that said connection must simultaneously act as a hinge and as a bilateral support. In this respect it must allow free rotation of the shovel portion about a transverse-horizontal axis, but must hinder movements between the plate and ski
20 in a vertical direction but must allow relative sliding in a longitudinal direction. It must hence be a hinge (of transverse-horizontal axis), to allow freedom of rotation between the shovel portion and said plate end, but must be horizontally slotted to also allow its relative longitudinal sliding; it can hence be defined as a slotted hinge.

This superstructure is therefore provided with at least three separate points of application to the ski, one of which is situated in a position 6 which is significantly advanced (with respect to the front jaw), possibly and preferably around the middle of the portion between the front jaw P and the section 4 where
5 the curvature of the tip commences. Consequently when the ski counter-flexes, the dynamic load F exerted by the skier is divided into at least three forces: two (F' , F'') or more acting on the base central region, and an additional force (F_{spat}) acting on said more advanced point 6.

It should be noted that the most significant role of this superstructure is not
10 merely to damp and absorb vibrations, although it undoubtedly and effectively performs this valuable accessory function. Its main role is to exert a supplementary reactive thrust F_{spat} on the point 6, to induce an elastic compensation effect thereat to significantly modify its counter-flexure deformation; it hence achieves the desired effect on the elastic deformation and on the related
15 distribution of the reaction load (Figure 4). It should however be noted that this effect is also substantially dependent on the elastic characteristics of the basic ski, which has to be adequately flexible particularly in the portion 7 below the arm 5.

The proposed configuration shown by way of example in Figures 6 and 7 can be subjected to suitable improvement. In this respect, to be applicable to any
20 ski it cannot be prefigured in a standardized form; it requires adaptation to the shape (in terms of the progression of the thicknesses and curvatures) of the ski for which it is intended. Moreover, the value of the thrust F_{spat} is strictly dependent on the flexibility of the arm and would be very difficult to regulate and preset (in order

to achieve a determined preload value and assume certain values increasing with the elastic counter-flexure deformation).

The aforesaid problem is radically simplified by using the following more evolved constructional variant (Figures 8-11).

- 5 The superstructure is no longer a single member but two members: a traditional base plate 10 and an independent semi-rigid front prolongation arm 11, i.e. a sort of rocker arm (Figure 8), as described hereinafter.

- 10 The prolongation arm 11, connected at its front to the slotted hinge 6, is connected at its rear to the front end of the base plate 10 by a hinge 12, it being also provided with a retro-prolongation 13 the end of which acts as a reaction element. Said end is provided with an element 14 of adjustable advancement (for example by means of a screw), which abuts against the base plate 10 (Figures 8, 9) or against the basic ski (Figures 10, 11), according to design requirements related to its elastic characteristics, by acting preferably on an interposed elastic or
15 semi-elastic element 15 (for example a high resistance rubber insert).

- It should be noted that in the second of the aforesaid cases, in which the design provides for the reaction element of the rocker arm to bear on the basic ski (Figures 10, 11), two supplementary forces act frontward through the rocker arm: in addition to the force F_{spat} , the force F'' exerted by the element 14 also acts on
20 the ski.

 As an alternative to the aforescribed proposed configurations, the base plate can be split into two half-plates, i.e. the superstructure portion below the boot comprises two distinct separated parts: a rear part 9 below the heel fixing unit, and a front part 8 below the sole. This latter provides all the aforescribed functional

aspects, as illustrated in Figure 12, which shows an extension of the structure already shown in Figure 8, and in Figure 13 which shows an extension of the structure shown in Figure 10.

Finally, the solution shown in Figures 8, 9 and the solution shown in
5 Figures 10, 11 can be simultaneously adopted (whether the base plate is whole or split), by simultaneously applying a first counteracting element 14 acting on the base plate, and a second counteracting element 16 acting on the ski, as shown in Figures 14 and 15.

A further embodiment (very particular, moreover for its simplicity), is
10 shown in Figures 16 and 17. It concerns exclusively the solution in which the base plate is fractioned into two different and separated parts 8 and 9. It involves only the front part 8 and it foresees the prolongation arm 5 to be integral part of it up to point 6 (fixed to the ski in the "slotted hinge" way as described and considered up to now). Said front plate portion (underneath the boot sole) is fixed to the central
15 region 1 of the ski through a transverse-horizontal axis solid hinge 17, at the rear with respect to the front jaw P. In this case the action F of the skier is transmitted to the ski by three forces: the F' one exerted on the heel fixing unit, the F_{spat} exerted by the end 6 of the arm and the F'' one exerted on the aforesaid hinge.

Independently of the embodiment used, the ski of the invention is
20 particularly advantageous by demonstrating an adequate flexibility combined with good distribution of the reaction load.

The superstructure of the ski according to the invention can be constructed of traditional materials or, advantageously, of different materials such

as composites, magnesium alloys, or monostructural hybrids which enable a specific weight reduction to be obtained for equal strength characteristics.

In addition, the superstructure can be produced using economical industrial pressing, forging and moulding techniques.